

BRL
1352
c.1A

BRLR 1352

BRL

AD 648644

EE NOV 1966

CIRCULATING COPY

REPORT NO. 1352

PARAMETRIC REPRESENTATIONS OF NON-STEADY
ONE-DIMENSIONAL FLOWS: A CORRECTION

by

J. H. Glese

PROPERTY OF U.S. ARMY
STINCO BRANCH
BRL, APG, MD. 21005

January 1967

Distribution of this document is unlimited.

U. S. ARMY MATERIEL COMMAND
BALLISTIC RESEARCH LABORATORIES
ABERDEEN PROVING GROUND, MARYLAND

Destroy this report when it is no longer needed.
Do not return it to the originator.

The findings in this report are not to be construed as
an official Department of the Army position, unless
so designated by other authorized documents.

BALLISTIC RESEARCH LABORATORIES

REPORT NO. 1352

JANUARY 1967

Distribution of this document is unlimited.

PARAMETRIC REPRESENTATIONS OF
NON-STEADY ONE-DIMENSIONAL FLOWS:
A CORRECTION

J. H. Giese

Computing Laboratory

PROPERTY OF U.S. ARMY
STINFO BRANCH
BRL, APG, MD. 21005

RDT&E Project No. 1P014501A14B

ABERDEEN PROVING GROUND, MARYLAND

INTENTIONALLY LEFT BLANK.

BALLISTIC RESEARCH LABORATORIES

REPORT NO. 1352

JHGiese/blk
Aberdeen Proving Ground, Md.
January 1967

PARAMETRIC REPRESENTATIONS OF NON-STEADY
ONE-DIMENSIONAL FLOWS: A CORRECTION

ABSTRACT

BRL Report No. 1316 contains a serious logical error. This invalidates that Report's assertions about the ease with which examples of 1-dimensional flows can be constructed. The present Report (i) expurgates BRL Report No. 1316 ; (ii) describes the error; (iii) corrects it; and (iv) salvages a family of examples of 1-dimensional flows.

INTENTIONALLY LEFT BLANK.

TABLE OF CONTENTS

	Page
ABSTRACT.	3
1. INTRODUCTION	7
2. THE FALLACY IN [1].	9
3. ON THE DETERMINATION OF $H(\alpha, \beta)$	11
4. FLOWS ASSOCIATED WITH $\xi = K(p) + L(\psi)$	17
5. SEPARABLE SOLUTIONS	20
6. BOTH X^+ , Y^+ AND X^- , Y^- ARE FUNCTIONALLY DEPENDENT	25
REFERENCES	27
DISTRIBUTION LIST.	29

INTENTIONALLY LEFT BLANK.

1. INTRODUCTION

Our recently published report [1]^{*} contains a fundamental logical error which invalidates our assertions about the ease with which certain parametric representations of non-steady one-dimensional flows could be constructed. Of course, this grievously restricts the prospects for application of such representations.

In this note we shall (i) expurgate [1]; (ii) describe our error; (iii) correct it; and (iv) develop a family of correct examples of our parametric representations.

The following changes are required in [1]:

Section 1: Delete the last three paragraphs.

Section 4: Delete all material starting with the paragraph that contains equation (4.9) and continuing to the end of Case 1.

Section 5: Delete the last paragraph.

Sections 6 to 8: Proposals to apply the method suggested in Section 4 are absurd and should be deleted.

The nature of our error can be summarized as follows. One dimensional flows can be characterized by means of solutions of a family of Monge-Ampère equations that involve a single non-constant coefficient, determined by the equation of state and by the form of the distribution of entropy among the various particle paths. By means of this coefficient we can subdivide the set of one-dimensional flows into mutually exclusive subsets. If we consider any two flows of the same subset we can identify the values of times, geometrical coordinates, and flow functions that correspond to identical values of the pressure, p , and of a Lagrangian variable, ψ . The

^{*}References in brackets may be found on page 27.

mapping of one up-plane onto another, defined in this way, preserves area. A well-known representation of the general area-preserving in terms of two parameters, α and β , involves an arbitrary function $H(\alpha, \beta)$. In attempting to apply this result to the comparison of two flows in the same subset, we determined a necessary condition that relates $H(\alpha, \beta)$ to a function $z(p, \psi)$ such that $\alpha = z_p$ and $\beta = z_\psi$. We assumed, erroneously, that $H(\alpha, \beta)$ remains arbitrary in our application. A necessary and sufficient condition, which will be developed in this note, restricts the permissible function $H(\alpha, \beta)$ to be any solutions of a certain quasi-linear, second order, hyperbolic partial differential equation.

It is not easy to guess solutions for the equation that defines H . Nevertheless, our representation retains a little value as a source of novelties, since for an important class of equations of state, which includes that of the perfect gases, we have been able to determine a family of separated-variable solutions of a suitably transformed version of the equation for H .

2. THE FALLACY IN [1]

We shall require the following extract from the valid and relevant parts of [1].

M. H. Martin [2] has developed the following formulation for the equations of all one-dimensional flows, except for an easily discussed special class. Let us define a Lagrangian variable, ψ , by

$$d\psi = \rho dx - \rho u dt . \quad (2.1)$$

Then the specific entropy must be of the form

$$s = s(\psi) , \quad (2.2)$$

and by the equation of state we can express the density in the form

$$\rho = \rho(p, s(\psi)) . \quad (2.3)$$

Assume that p and ψ are functionally independent, and let

$\xi(p, \psi)$ be any solution of

$$\xi_{pp}\xi_{\psi\psi} - \xi_{p\psi}^2 = -A^2(p, \psi) , \quad (2.4)$$

where

$$A^2(p, \psi) = - (1/\rho)_p \neq 0 . \quad (2.5)$$

Then the description of a one-dimensional flow is completed by

$$t = \xi_p , \quad u = \xi_\psi , \quad (2.6)$$

$$dx = \xi_\psi d\xi_p + (1/\rho)d\psi , \quad (2.7)$$

where t denotes time, u particle velocity and x an Eulerian coordinate.

Now let us suppose $\xi(p, \psi)$ and $\xi^*(p, \psi)$ are two different solutions of (2.4) that correspond to the same $A(p, \psi)$. The mapping of the $u^* t^*$ -plane onto the $u t$ -plane, defined by identifying points with identical values of p and ψ preserves area. Hence we must have

$$\xi_p = \alpha + H_\beta \quad , \quad \xi_\psi = \beta - H_\alpha \quad , \quad (2.8)$$

$$\xi_p^* = \alpha - H_\beta \quad , \quad \xi_\psi^* = \beta + H_\alpha \quad , \quad (2.9)$$

for some function $H(\alpha, \beta)$ of some parameters α and β . Since we are actually interested in t^* and u^* , rather than ξ^* for its own sake, it would suffice to determine an acceptable H , or even just H_α and H_β . If we set

$$2z(p, \psi) = \xi + \xi^* \quad , \quad 2w(p, \psi) = \xi - \xi^* \quad , \quad (2.10)$$

then by (2.8) to (2.10)

$$\alpha = z_p \quad , \quad \beta = z_\psi \quad , \quad (2.11)$$

$$H_\alpha = -w_\psi \quad , \quad H_\beta = w_p \quad . \quad (2.12)$$

If we eliminate w from (2.12) we obtain

$$\left(\frac{\partial}{\partial p} \frac{\partial}{\partial z_p} + \frac{\partial}{\partial \psi} \frac{\partial}{\partial z_\psi} \right) H(z_p, z_\psi) = 0 \quad . \quad (2.13)$$

Up to this point in [1] all of our reasoning has been legitimate.

In [1] we assumed that H was arbitrary. This is incorrect since, as we shall show in the following section, $H(\alpha, \beta)$ must satisfy the quasi-linear partial differential equation (3.16).

3. ON THE DETERMINATION OF $H(\alpha, \beta)$.

Let us continue to assume that $\xi(p, \psi)$ is a known solution of (2.4) for a given $A(p, \psi) \neq 0$. Recall that by (2.6), (2.8), and (2.11) we have

$$\xi_p(p, \psi) = t = \alpha + H_\beta, \quad \xi_\psi(p, \psi) = u = \beta - H_\alpha, \quad (3.1)$$

and

$$\alpha = z_p(p, \psi), \quad \beta = z_\psi(p, \psi), \quad (3.2)$$

for some $H(\alpha, \beta)$ and $z(p, \psi)$. Since ξ_p and ξ_ψ are functionally independent by (2.4), (3.1) implicitly defines

$$p = p(t, u), \quad \psi = \psi(t, u). \quad (3.3)$$

Since the functions (3.3) are the inverses of the functions (3.1), we must have

$$\begin{pmatrix} \xi_{pp} & \xi_{p\psi} \\ \xi_{p\psi} & \xi_{\psi\psi} \end{pmatrix}^{-1} = \begin{pmatrix} p_t & p_u \\ \psi_t & \psi_u \end{pmatrix}.$$

Thus

$$p_t/\xi_{\psi\psi} = -\psi_t/\xi_{p\psi} = -p_u/\xi_{p\psi} = \psi_u/\xi_{pp}. \quad (3.4)$$

By (3.1) and (3.3) we can express p and ψ as functions of α and β . Since we have assumed that p and ψ are independent, then α and β must also be independent. Now let us make the Legendre transformation defined by (3.2) and

$$Z(\alpha, \beta) = pz_p + \psi z_\psi - z = \alpha p + \beta \psi - z. \quad (3.5)$$

Then we must have

$$p = Z_{\alpha} \quad , \quad \psi = Z_{\beta} \quad , \quad (3.6)$$

and now by (3.5) and (3.6)

$$z(p, \psi) = \alpha Z_{\alpha} + \beta Z_{\beta} - Z = \alpha p + \beta \psi - Z \quad . \quad (3.7)$$

Furthermore, by a well-known property of Legendre transformations

$$z_{pp}/Z_{\beta\beta} = - z_{p\psi}/Z_{\alpha\beta} = z_{\psi\psi}/Z_{\alpha\alpha} \quad . \quad (3.8)$$

By (3.1) and (3.6) we have

$$\begin{aligned} \xi_p(Z_{\alpha}, Z_{\beta}) &= \alpha + H_{\beta} \quad , \\ \xi_{\psi}(Z_{\alpha}, Z_{\beta}) &= \beta - H_{\alpha} \quad . \end{aligned} \quad (3.9)$$

For a known $\xi(p, \psi)$ let the pair $H(\alpha, \beta)$, $Z(\alpha, \beta)$ be any solution of the system (3.9). Define p and ψ by (3.6) and $z(p, \psi)$ by (3.7). Then (3.2) follows from the Legendre transformation (3.6) and (3.7). Finally, (3.9) and (3.6) imply (3.1). Thus (3.1) and (3.2) are equivalent to (3.6) and (3.9).

If we eliminate H from (3.9) we obtain

$$(\xi_p - \alpha)_{\alpha} + (\xi_{\psi} - \beta)_{\beta} = 0 \quad , \quad (3.10)$$

which is equivalent to

$$\xi_{pp} Z_{\alpha\alpha} + 2\xi_{p\psi} Z_{\alpha\beta} + \xi_{\psi\psi} Z_{\beta\beta} = 2 \quad , \quad (3.11)$$

where the arguments of ξ_{pp} , $\xi_{p\psi}$, and $\xi_{\psi\psi}$ have been replaced by the expressions (3.6). In general, (3.11) is a non-linear partial differential equation for $Z(\alpha, \beta)$. By (2.4) it is of hyperbolic type.

If we let $Z(\alpha, \beta)$ be any solution of (3.11) such that Z_α and Z_β are independent, and if we define p and ψ by (3.6), then (3.11) is equivalent to (3.10). This, in turn, implies (3.9) for some $H(\alpha, \beta)$. A possible $H(\alpha, \beta)$ could be defined by

$$H(\alpha, \beta) = \int \left[(\xi_p - \alpha) d\beta - (\xi_\psi - \beta) d\alpha \right] . \quad (3.12)$$

If we know a solution $Z(\alpha, \beta)$, we need not actually determine $H(\alpha, \beta)$. For, by (2.8), (2.9), and (2.11)

$$\xi^*(p, \psi) = 2z(p, \psi) - \xi(p, \psi) . \quad (3.13)$$

To determine $\xi^*(p, \psi)$, it would suffice to find $z(p, \psi)$. But the latter can be defined by (3.7).

Instead of eliminating H from (3.9), let us solve for Z_α and Z_β to obtain

$$\begin{aligned} Z_\alpha &= p(\alpha + H_\beta, \beta - H_\alpha) , \\ Z_\beta &= \psi(\alpha + H_\beta, \beta - H_\alpha) , \end{aligned} \quad (3.14)$$

in terms of the inverse functions p and ψ defined by (3.3). If we eliminate Z from (3.14) we obtain

$$\frac{\partial p}{\partial \beta} - \frac{\beta \psi}{\beta \alpha} = 0 , \quad (3.15)$$

or in expanded form

$$p_t H_{\beta\beta} + p_u (1 - H_{\alpha\beta}) - \psi_t (1 + H_{\alpha\beta}) + \psi_u H_{\alpha\alpha} = 0 \quad .$$

By (3.4) this becomes

$$\xi_{pp} H_{\alpha\alpha} + 2\xi_{p\psi} H_{\alpha\beta} + \xi_{\psi\psi} H_{\beta\beta} = 0 \quad (3.16)$$

If we replace the arguments of ξ_{pp} , $\xi_{p\psi}$, and $\xi_{\psi\psi}$ by the right members of (3.14), (3.16) becomes a quasi-linear partial differential equation for $H(\alpha, \beta)$. All steps from (3.14) to (3.16) are reversible. Hence, for any solution H of (3.16) there exists a $Z(\alpha, \beta)$ which satisfies (3.14).

The problem of constructing a new solution $\xi^*(p, \psi)$ of (2.4) from a previously determined solution $\xi(p, \psi)$ has been transformed into that of solving the quasi-linear equation (3.16). For most equations of state (3.16) will still be non-linear. Thus nothing has been gained unless we can at least guess some solutions $H(\alpha, \beta)$. This will be done in Sections 4 and 5 for an important special class of flows.

In our discussion up to this point we have assumed $\xi(p, \psi)$ is known. As a by-product we have discovered the parametric representation (3.1), (3.6) for t, u, p, ψ in terms of suitable functions $H(\alpha, \beta)$ and $Z(\alpha, \beta)$. Prior knowledge of $\xi(p, \psi)$ is not really essential for this parametric representation, since we can determine a system of partial differential equations for H and Z that does not depend on ξ . First, note that by (2.4) we must have

$$\frac{\partial(\xi_p, \xi_\psi)}{\partial(\alpha, \beta)} = -A^2(p, \psi) \frac{\partial(p, \psi)}{\partial(\alpha, \beta)} .$$

By (3.1) and (3.6) this is equivalent to

$$H_{\alpha\alpha}H_{\beta\beta} - H_{\alpha\beta}^2 + 1 = -A^2(Z_\alpha, Z_\beta)(Z_{\alpha\alpha}Z_{\beta\beta} - Z_{\alpha\beta}^2) \quad (3.17)$$

On the other hand, if we eliminate ξ from (3.1), we obtain

$$(\alpha + H_\beta)_\psi - (\beta - H_\alpha)_p = 0 .$$

In expanded form this becomes

$$(1 + H_{\alpha\beta})\alpha_\psi + H_{\beta\beta}\beta_\psi + H_{\alpha\alpha}\alpha_p - (1 - H_{\alpha\beta})\beta_p = 0 ,$$

whence by (3.2) and (3.8)

$$Z_{\beta\beta}H_{\alpha\alpha} - 2Z_{\alpha\beta}H_{\alpha\beta} + Z_{\alpha\alpha}H_{\beta\beta} = 0 . \quad (3.18)$$

Thus, in the present case the pair H, Z must be a solution of the system (3.17), (3.18).

To complete our parametric representation note that by (2.7), (3.1), and (3.6).

$$\begin{aligned} x_\alpha &= (\beta - H_\alpha) (1 + H_{\alpha\beta}) + \rho^{-1} Z_{\alpha\beta} , \\ x_\beta &= (\beta - H_\alpha) H_{\beta\beta} + \rho^{-1} Z_{\beta\beta} . \end{aligned} \quad (3.19)$$

It might be worth mentioning that for $H \equiv \text{constant}$ (3.18) is certainly satisfied. By (3.1) we have

$$\alpha = t = \xi_p, \quad \beta = u = \xi_\psi. \quad (3.20)$$

Now (3.2) yields

$$\xi = z \quad (3.21)$$

and (3.6) becomes

$$Z(t, u) = pt + \beta u - \xi. \quad (3.22)$$

Then (3.17) reduces, as one would expect, to the equation that would be obtained from (2.4) under the Legendre transformation (3.20), (3.22).

4. FLOWS ASSOCIATED WITH $\xi = K(p) + L(\psi)$

Equation (2.4) will have the solution

$$\xi = K(p) + L(\psi) \quad (4.1)$$

if

$$-A^2(p, \psi) = K''(p) L''(\psi) , \quad (4.2)$$

where primes denote differentiation with respect to the appropriate argument, and by (2.5)

$$K''(p) L''(\psi) \neq 0 . \quad (4.3)$$

By (2.5) this choice of A^2 corresponds to

$$\rho = 1/[K'(p)L''(\psi) + M(\psi)] , \quad (4.4)$$

where $M(\psi)$ is an arbitrary function of ψ . If

$$\psi = \psi(s) \quad (4.5)$$

is the inverse of the function $s(\psi)$ mentioned in (2.2), then (4.4)

and (4.5) define an equation of state. The equation of state of a perfect gas,

$$\rho/\rho_0 = e^{-s/c_p} (p/p_0)^{1/\gamma} ,$$

is in the class defined by (4.4) for $M = 0$.

By (4.1) equation (3.16) assumes the form

$$K''(p) H_{\alpha\alpha} + L''(\psi) H_{\beta\beta} = 0 , \quad (4.6)$$

where by (2.8)

$$K'(p) = \alpha + H_{\beta} , \quad L'(\psi) = \beta - H_{\alpha} . \quad (4.7)$$

By (4.3) equations (4.7) uniquely define

$$p = p(\alpha + H_\beta) , \quad \psi = \psi(\beta - H_\alpha) . \quad (4.8)$$

Since (4.6) is non-linear we cannot hope to find the general solution for arbitrary choices of K'' and L'' . However, we can develop some particular solutions, as follows.

First, it will be convenient to make one of the transformations

$$X^\pm = \alpha \pm H_\beta , \quad Y^\pm = \beta \pm H_\alpha , \quad (4.9)$$

$$Z^\pm = 2(\alpha\beta \mp H) - P^\pm Q^\pm , \quad (4.10)$$

$$P^\pm = \beta \mp H_\alpha , \quad Q^\pm = \alpha \mp H_\beta , \quad (4.11)$$

Then

$$\xi_p = K'(p) = X, \quad \xi_\psi = L'(\psi) = P, \quad \xi_p^* = Q, \quad \xi_\psi^* = Y \quad (4.12+)$$

for + superscripts, and

$$\xi_p = K'(p) = Q, \quad \xi_\psi = L'(\psi) = Y, \quad \xi_p^* = X, \quad \xi_\psi^* = P \quad (4.12-)$$

for - superscripts.

In the sequel we shall assume that one of the pairs X^+, Y^+ or X^-, Y^- is functionally independent. The exceptional case in which both pairs are functionally dependent will be discussed in Section 6.

For convenience we shall omit the superscripts hereafter.

It can easily be verified that $dZ = PdX + QdY$, so that

$$P = Z_X , \quad Q = Z_Y ,$$

and then

$$\begin{aligned} dP &= Z_{XX}dX + Z_{XY}dY \quad , \\ dQ &= Z_{XY}dX + Z_{YY}dY \quad . \end{aligned} \tag{4.13}$$

From (4.9) to (4.12) we obtain

$$1 \mp H_{\alpha\beta} - (1 \pm H_{\alpha\beta}) Z_{XY} = \pm Z_{XX} H_{\beta\beta} = \pm Z_{YY} H_{\alpha\alpha}$$

Eliminate $H_{\alpha\alpha}$ and $H_{\beta\beta}$ from the latter of these equations and (4.6) to find either

$$K''(p(X))Z_{XX} + L''(\psi(P))Z_{YY} = 0 \tag{4.14+}$$

for + superscripts, or

$$K''(p(Q))Z_{XX} + L''(\psi(Y))Z_{YY} = 0 \tag{4.14-}$$

for - superscripts.

5. SEPARABLE SOLUTIONS

Now let us try to find solutions of (4.14-) of the form

$$Z(X, Y) = k(X) \ell(Y) . \quad (5.1)$$

As we shall eventually discover, this will impose a strong, but acceptable, restriction on the permissible functional forms for $K(p)$.

By (5.1)

$$P = k'(X)\ell(Y) , \quad Q = k(X)\ell'(Y) . \quad (5.2)$$

By (4.7) and (4.9) for - superscripts

$$K'(p) = Q , \quad L'(\psi) = Y , \quad (5.3)$$

whence

$$p = p(Q) , \quad \psi = \psi(Y) . \quad (5.4)$$

Now (4.14-) yields

$$K''(p(Q))k''(X)\ell(Y) + L''(\psi(Y))k(X)\ell''(Y) = 0 . \quad (5.5)$$

Next, we may assume Q and X are independent. For, if they were not, then by (4.12-) and (2.6) ξ_p and ξ_p^* would be dependent. Since $t^* = \xi_p^*$ must not be constant, we would have $\xi_p^* = G(\xi_p)$ for some non-constant function G . Hence

$$\xi_{p\psi}^* = G'(\xi_p) \xi_{p\psi} = 0$$

by (4.1). Hence $\xi^* = K^*(p) + L^*(\psi)$. Since solutions of this form have been considered in [1], this requires no further discussion.

Incidentally, if Q and X are independent, then by (5.2) $k \ell' \neq 0$, and hence $k \ell \neq 0$, in general. Then we can rewrite (5.5) as

$$K''(p(Q)) \frac{k''(X)}{k(X)} + \frac{L''(\psi(Y)) \ell''(Y)}{\ell(Y)} = 0 . \quad (5.6)$$

Differentiate the left-hand member of (5.6) with respect to X , and use (5.2) to find

$$\frac{K'''(p)p'(Q)Q}{K''(p)} = - \frac{k(X)}{k'(X)} \left[\log \frac{k''(X)}{k(X)} \right]' = c_1 . \quad (5.7)$$

By (5.3)

$$K''(p)p'(Q) = 1 , \quad L''(\psi)\psi'(Y) = 1 . \quad (5.8)$$

Thus (5.3) and the outer members of (5.7) yield

$$K'''(p)/K''(p) = c_1 K''(p)/K'(p) ,$$

whence

$$K''(p) = c_2 K'^{c_1}(p) . \quad (5.9)$$

CASE 1 : If $c_1 = 1$, then (5.9) implies

$$K(p) = c_3 e^{c_2 p} + c_4 , \quad (5.10)$$

whence

$$K''(p) = c_2^2 c_3 e^{c_2 p} = c_2 K'(p) = c_2 Q , \quad (5.11)$$

and then

$$p = \frac{1}{c_2} \log \frac{Q}{c_2 c_3} . \quad (5.12)$$

Now (5.5) yields

$$\frac{L''(\psi) \ell''(Y)}{\ell(Y) \ell'(Y)} = - c_2 k''(X) = c_5 . \quad (5.13)$$

Then by (5.8) and (5.13) k and ℓ must satisfy

$$k(X) = -\frac{c_5}{2c_2} X^2 + c_6 X + c_7 \quad , \quad (5.14)$$

$$\ell''(Y) = c_5 \psi'(Y) \ell(Y) \ell'(Y) \quad , \quad (5.15)$$

where $\psi(Y)$ is defined by (5.3) .

Note that although the choice of $K(p)$ is restricted by (5.10), the choice of $L(\psi)$ is arbitrary. Any solution of (5.15) with $\ell'' \neq 0$ can be multiplied by any polynomial (5.14) with $c_5 \neq 0$ to form a product solution Z of (4.14-). Then (4.12-) will enable us to construct a ξ^* that differs from ξ in the following important respect. By (4.1)

$$\xi_{p\psi} = 0 \quad . \quad (5.16)$$

On the other hand, by (4.12-) and (5.2)

$$\xi_{\psi}^* = P = k'(X) \ell(L'(\psi)) \quad .$$

By (5.2) and (5.3)

$$K'(p) = Q = k(X) \ell'(L'(\psi)) \quad .$$

Since by (5.8) $K'' \neq 0$, then by (5.14) with $c_5 \neq 0$ this actually suffices to define a function $X(p, \psi)$ such that $X_p \neq 0$. But then

$$\xi_{\psi p}^* = k'' \ell(L'(\psi)) X_p \neq 0$$

in contrast with (5.16). Thus ξ^* is not a completely trivial modification of ξ .

CASE 2: Now suppose $c_1 \neq 1$. By (5.9)

$$K(p) = \frac{1}{c_2(2-c_1)} \left[(1-c_1)c_2(p+c_3) \right]^{\frac{2-c_1}{1-c_1}} + c_4, \quad (5.17)$$

$$Q = K'(p) = \left[(1-c_1)c_2(p+c_3) \right]^{\frac{1}{1-c_1}} \quad (5.18)$$

$$K''(p) = c_2 Q^{c_1}. \quad (5.19)$$

Now (5.2), (5.5), and (5.19) yield

$$\frac{L''(\psi)\ell''(Y)}{\ell(Y)\ell'^{c_1}(Y)} = -c_2 k^{c_1-1}(X)k''(X) = c_5. \quad (5.20)$$

Then by (5.8) and (5.20) we obtain

$$k''(X) = -c_2^{-1} c_5 k^{1-c_1}(X), \quad (5.21)$$

$$\ell''(Y) = c_5 \psi'(Y) \ell(Y) \ell'^{c_1}(Y). \quad (5.22)$$

Equation (5.21) can be solved by quadratures, of course.

Again, the choice of $K(p)$ is restricted, this time by (5.17), but $L(\psi)$ is still arbitrary. The restriction on the form of $K(p)$ is not too serious, if we note that for $c_3 = 0$, $c_1 = \gamma + 1$, $M(\psi) = 0$, and arbitrary $L(\psi)$, (5.18) and (4.4) lead to the equation of state for a perfect gas.

By the argument presented at the end of Case 1, $\xi_{\psi p}^* \neq 0$ again.

All of the discussion in this section has dealt with (4.14-). A similar analysis of separable solutions could be developed for (4.14+). All that we really require are the analogs of equations (5.10), (5.14), and (5.15), or of (5.17), (5.21), and (5.22). These can easily be written by interchanging X and Y ; k and ℓ ; K and L ; and p and ψ . Now, of course, it becomes possible to choose $K(p)$ arbitrarily, but then $L(\psi)$ is restricted. This situation seems to have less physical interest than the one we have just discussed at length.

6. BOTH X^+ , Y^+ AND X^- , Y^- ARE FUNCTIONALLY
DEPENDENT

If both X^+ , Y^+ and X^- , Y^- are functionally dependent, then in accordance with (4.9)

$$\partial(\alpha \pm H_\beta, \beta \pm H_\alpha) / \partial(\alpha, \beta) = 0 . \quad \text{Thus}$$

$$(1 \pm H_{\alpha\beta})^2 - H_{\alpha\alpha} H_{\beta\beta} = 0 .$$

These equations are equivalent to

$$H_{\alpha\beta} = 0 , \quad (6.1)$$

$$H_{\alpha\alpha} H_{\beta\beta} = 1 . \quad (6.2)$$

By (6.1)

$$H(\alpha, \beta) = f(\alpha) + g(\beta) , \quad (6.3)$$

for some $f(\alpha)$ and $g(\beta)$. By (6.2) $f''(\alpha)g''(\beta) = 1$, whence

$$f'' = c_1 , \quad g'' = 1/c_1 .$$

Thus

$$f(\alpha) = \frac{1}{2} c_1 \alpha^2 + c_2 \alpha + c_3 , \quad (6.4)$$

$$g(\beta) = \frac{1}{2c_1} \beta^2 + c_4 \beta + c_5 . \quad (6.5)$$

By (2.11) we can rewrite (2.8) in the form

$$(\xi - z)_p = H_\beta = g'(\beta) = \frac{1}{c_1} (z + c_1 c_4 \psi)_\psi ,$$

$$(\xi - z)_\psi = -H_\alpha = -f'(\alpha) = -c_1 (z + \frac{c_2}{c_1} p)_p .$$

Hence

$$\xi - z + i(z + \frac{c_2}{c_1} p + c_1 c_4 \psi) = f(\zeta) \quad (6.6)$$

where $f(\zeta)$ is an analytic function of the complex variable

$$\zeta = p + i c_1 \psi . \quad (6.7)$$

Thus

$$\xi_{pp} + c_1^{-2} \xi_{\psi\psi} = 0 .$$

If we demand that ξ be of the form (4.1), then

$$K''(p) = -c_1^{-2} L''(\psi) = c_6 . \quad \text{Then by (4.1) and (2.4) to (2.7)}$$

$$t = \xi_p = c_6 p + c_7 ,$$

$$u = \xi_\psi = -c_1^2 c_6 \psi + c_8 ,$$

$$A^2 = c_1^2 c_6^2 ,$$

$$1/\rho = -c_1^2 c_6^2 p + M(\psi) ,$$

$$x = -c_1^2 c_6^2 p\psi + c_6 c_{10} p + \int M(\psi) d\psi .$$

This corresponds to a class of flows with straight particle paths on which the velocity is constant (though it varies from path to path).

J. H. GIESE

REFERENCES

1. Giese, J. H., Parametric Representations of Non-Steady One-Dimensional Flows, BRL Report No. 1316; J. Math. Analysis and Applications 15(1966), 397-420 .
2. Martin, M. H., The Propagation of a Plane Shock into a Quiet Atmosphere, Can. J. Math. 5(1953), 37-39 .

INTENTIONALLY LEFT BLANK.

DISTRIBUTION LIST

<u>No. of</u> <u>Copies</u>	<u>Organization</u>	<u>No. of</u> <u>Copies</u>	<u>Organization</u>
20	Commander Defense Documentation Center ATTN: TIPCR Cameron Station Alexandria, Virginia 22314	3	Commander U.S. Naval Air Systems Command Headquarters ATTN: AIR-604 Washington, D.C. 20360
1	Director of Defense Research and Engineering (OSD) Washington, D.C. 20301	1	Commanding Officer & Director David W. Taylor Model Basin Washington, D.C. 20007
1	Director Advanced Research Projects Agency ATTN: CDR G. Dickey Department of Defense Washington, D.C. 20301	1	Commander U.S. Naval Missile Center Point Mugu, California 93041
1	Commanding General U.S. Army Materiel Command ATTN: AMCRD-TE Washington, D.C. 20315	3	Commander U.S. Naval Ordnance Laboratory ATTN: Dr. J. Enig (1 cy) Silver Spring, Maryland 20910
2	Commanding Officer U.S. Army Engineer Research and Development Laboratories ATTN: STINFO Div SMEFB-MG Fort Belvoir, Virginia 22060	1	Commander U.S. Naval Weapons Laboratory Dahlgren, Virginia 22448
1	Commanding Officer U.S. Army Picatinny Arsenal ATTN: SMUPA-VE Dover, New Jersey 07801	2	AFATL (ATWR, Mr. Dittrich, Mr. Howard) Eglin AFB Florida 32542
1	Commanding Officer U.S. Army Engineer Waterways Experiment Agency ATTN: Dr. A. Sakurai Vicksburg, Mississippi 39180	1	AFCRL L. G. Hanscom Fld Bedford, Massachusetts 01731
1	Director U.S. Army Research Office ATTN: CRDPES, Dr. I. Hershner 3045 Columbia Pike Arlington, Virginia 22204	1	AFWL (WLL) Kirtland AFB New Mexico 87117
		1	Director National Bureau of Standards ATTN: Dr. W. H. Pell U.S. Department of Commerce Washington, D.C. 20234
		1	Headquarters U.S. Atomic Energy Commission ATTN: Div of Tech Info Washington, D.C. 20545

DISTRIBUTION LIST

<u>No. of</u> <u>Copies</u>	<u>Organization</u>	<u>No. of</u> <u>Copies</u>	<u>Organization</u>
2	Director Lawrence Radiation Laboratory University of California ATTN: Dr. W. Noh Mr. M. Wilkins P.O. Box 808 Livermore, California 94551	1	Director National Aeronautics and Space Administration Lewis Research Center 21000 Brookpark Road Cleveland, Ohio 44135
1	Director Los Alamos Scientific Laboratory University of California P.O. Box 1663 Los Alamos, New Mexico 87544	1	AVCO Corporation Research and Advanced Development Division 201 Lowell Street Wilmington, Massachusetts 01887
1	Director NASA Scientific and Technical Information Facility ATTN: SAK/DL P.O. Box 33 College Park, Maryland 20740	1	Battelle Memorial Institute 505 King Street Columbus, Ohio 43201
2	Director National Aeronautics and Space Administration Ames Research Center ATTN: Mr. J. Summers MS 223-1 Lib Br, MS 202-3 Moffett Field, California 94035	2	Firestone Tire and Rubber Company ATTN: Lib Mr. M. Cox 1200 Firestone Parkway Akron, Ohio 44317
1	Director National Aeronautics and Space Administration Goddard Space Flight Center ATTN: Code 252, Tech Lib Greenbelt, Maryland 20771	2	General Dynamics Corporation General Atomic Division ATTN: Mr. M. Scharff Dr. J. Walsh P.O. Box 1111 San Diego, California 92112
1	Director National Aeronautics and Space Administration Langley Research Center Langley Station Hampton, Virginia 23365	1	General Electric Company Missile and Space Division ATTN: Mr. Howard Semon P.O. Box 8555 Philadelphia, Pennsylvania 19101
		2	General Motors Corporation Defense Research Laboratories ATTN: Mr. J. Gehring Dr. A. Charters Santa Barbara, California 93108

DISTRIBUTION LIST

<u>No. of</u> <u>Copies</u>	<u>Organization</u>	<u>No. of</u> <u>Copies</u>	<u>Organization</u>
1	The Martin Company ATTN: Sc Tech Lib Baltimore, Maryland 21203	1	Professor W. F. Ames University of Delaware Newark, Delaware 19711
1	The Martin Company Aerospace Division Orlando, Florida 32805	1	Professor G. Birkhoff Harvard University Cambridge, Massachusetts 02138
1	The Rand Corporation 1700 Main Street Santa Monica, California 90406	1	Professor G. Carrier Division of Engineering and Applied Physics Harvard University Cambridge, Massachusetts 01238
1	Sandia Corporation ATTN: Info Dist Div P.O. Box 5800 Albuquerque, New Mexico 87115	1	Professor P. C. Chou Drexel Institute of Technology 32nd & Chestnut Streets Philadelphia, Pennsylvania 19104
1	Shock Hydrodynamics, Inc. ATTN: Dr. L. Zernow 15010 Ventura Boulevard Sherman Oaks, California 91403	1	Professor N. Davids Department of Engineering Mechanics The Pennsylvania State University University Park, Pennsylvania 16802
1	United Aircraft Corporation Missiles & Space Systems Group Hamilton Standard Division Windsor Locks, Connecticut 06096	1	Professor Paul Garabedian Courant Institute of Mathematical Sciences New York University 251 Mercer Street New York, New York 10012
1	Brown University Division of Engineering Providence, Rhode Island 02912	1	Professor R. N. Gunderson University of Wisconsin Milwaukee, Wisconsin 53200
1	IIT Research Laboratories 10 West 35th Street Chicago, Illinois 60616	1	Professor M. Holt Aeronautical Sciences Division University of California Berkeley, California 94704
1	Lincoln Laboratory (MIT) 244 Wood Street Lexington, Massachusetts 02173	1	Professor G. S. S. Ludford Cornell University Ithaca, New York 14850
1	University of Utah High Velocity Laboratory Salt Lake City, Utah 84112		

DISTRIBUTION LIST

<u>No. of</u> <u>Copies</u>	<u>Organization</u>
1	Professor M. H. Martin University of Maryland College Park, Maryland 20740
1	Professor M. H. Protter University of California Berkeley, California 94704
1	Professor E. M. Pugh Department of Physics Carnegie Institute of Technology Pittsburgh, Pennsylvania 15213
1	Professor C. A. Truesdell Johns Hopkins University 34th & Charles Streets Baltimore, Maryland 21218
1	Dr. Michael Cowperthwaite Stanford Research Institute 333 Ravenswood Avenue Menlo Park, California 94025
1	Dr. M. W. Evans Stanford Research Institute 333 Ravenswood Avenue Menlo Park, California 94025
1	Dr. C. Grosch Davidson Laboratory Stevens Institute of Technology Castle Point Station Hoboken, New Jersey 07030

Aberdeen Proving Ground

Ch, Tech Lib
Air Force Ln Ofc
Marine Corps Ln Ofc
Navy Ln Ofc
CDC Ln Ofc

DOCUMENT CONTROL DATA - R&D

(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)

1. ORIGINATING ACTIVITY (Corporate author) U.S. Army Ballistic Research Laboratories Aberdeen Proving Ground, Maryland		2a. REPORT SECURITY CLASSIFICATION Unclassified	
		2b. GROUP	
3. REPORT TITLE PARAMETRIC REPRESENTATIONS OF NON-STEADY ONE-DIMENSIONAL FLOWS: A CORRECTION			
4. DESCRIPTIVE NOTES (Type of report and inclusive dates)			
5. AUTHOR(S) (Last name, first name, initial) Giese, J. H.			
6. REPORT DATE January 1967		7a. TOTAL NO. OF PAGES 32	7b. NO. OF REFS 2
8a. CONTRACT OR GRANT NO.		9a. ORIGINATOR'S REPORT NUMBER(S) Report No. 1352	
b. PROJECT NO. RDT&E 1P014501A14B			
c.		9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report)	
d.			
10. AVAILABILITY/LIMITATION NOTICES Distribution of this document is unlimited.			
11. SUPPLEMENTARY NOTES		12. SPONSORING MILITARY ACTIVITY U. S. Army Materiel Command Washington, D. C.	
13. ABSTRACT BRL Report No. 1316 contains a serious logical error. This invalidates that Report's assertions about the ease with which examples of 1-dimensional flows can be constructed. The present Report (i) expurgates BRL Report No. 1316; describes the error; (iii) corrects it; and (iv) salvages a family of examples of 1-dimensional flows.			

14. KEY WORDS	LINK A		LINK B		LINK C	
	ROLE	WT	ROLE	WT	ROLE	WT
One-dimensional flows Non-steady flows						

INSTRUCTIONS

1. **ORIGINATING ACTIVITY:** Enter the name and address of the contractor, subcontractor, grantee, Department of Defense activity or other organization (*corporate author*) issuing the report.

2a. **REPORT SECURITY CLASSIFICATION:** Enter the overall security classification of the report. Indicate whether "Restricted Data" is included. Marking is to be in accordance with appropriate security regulations.

2b. **GROUP:** Automatic downgrading is specified in DoD Directive 5200.10 and Armed Forces Industrial Manual. Enter the group number. Also, when applicable, show that optional markings have been used for Group 3 and Group 4 as authorized.

3. **REPORT TITLE:** Enter the complete report title in all capital letters. Titles in all cases should be unclassified. If a meaningful title cannot be selected without classification, show title classification in all capitals in parenthesis immediately following the title.

4. **DESCRIPTIVE NOTES:** If appropriate, enter the type of report, e.g., interim, progress, summary, annual, or final. Give the inclusive dates when a specific reporting period is covered.

5. **AUTHOR(S):** Enter the name(s) of author(s) as shown on or in the report. Enter last name, first name, middle initial. If military, show rank and branch of service. The name of the principal author is an absolute minimum requirement.

6. **REPORT DATE:** Enter the date of the report as day, month, year; or month, year. If more than one date appears on the report, use date of publication.

7a. **TOTAL NUMBER OF PAGES:** The total page count should follow normal pagination procedures, i.e., enter the number of pages containing information.

7b. **NUMBER OF REFERENCES:** Enter the total number of references cited in the report.

8a. **CONTRACT OR GRANT NUMBER:** If appropriate, enter the applicable number of the contract or grant under which the report was written.

8b, 8c, & 8d. **PROJECT NUMBER:** Enter the appropriate military department identification, such as project number, subproject number, system numbers, task number, etc.

9a. **ORIGINATOR'S REPORT NUMBER(S):** Enter the official report number by which the document will be identified and controlled by the originating activity. This number must be unique to this report.

9b. **OTHER REPORT NUMBER(S):** If the report has been assigned any other report numbers (*either by the originator or by the sponsor*), also enter this number(s).

10. **AVAILABILITY/LIMITATION NOTICES:** Enter any limitations on further dissemination of the report, other than those imposed by security classification, using standard statements such as:

- (1) "Qualified requesters may obtain copies of this report from DDC."
- (2) "Foreign announcement and dissemination of this report by DDC is not authorized."
- (3) "U. S. Government agencies may obtain copies of this report directly from DDC. Other qualified DDC users shall request through _____."
- (4) "U. S. military agencies may obtain copies of this report directly from DDC. Other qualified users shall request through _____."
- (5) "All distribution of this report is controlled. Qualified DDC users shall request through _____."

If the report has been furnished to the Office of Technical Services, Department of Commerce, for sale to the public, indicate this fact and enter the price, if known.

11. **SUPPLEMENTARY NOTES:** Use for additional explanatory notes.

12. **SPONSORING MILITARY ACTIVITY:** Enter the name of the departmental project office or laboratory sponsoring (*paying for*) the research and development. Include address.

13. **ABSTRACT:** Enter an abstract giving a brief and factual summary of the document indicative of the report, even though it may also appear elsewhere in the body of the technical report. If additional space is required, a continuation sheet shall be attached.

It is highly desirable that the abstract of classified reports be unclassified. Each paragraph of the abstract shall end with an indication of the military security classification of the information in the paragraph, represented as (TS), (S), (C), or (U).

There is no limitation on the length of the abstract. However, the suggested length is from 150 to 225 words.

14. **KEY WORDS:** Key words are technically meaningful terms or short phrases that characterize a report and may be used as index entries for cataloging the report. Key words must be selected so that no security classification is required. Identifiers, such as equipment model designation, trade name, military project code name, geographic location, may be used as key words but will be followed by an indication of technical context. The assignment of links, rules, and weights is optional.